Chemical synthesis of ceramic materials

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A range of increasingly important chemical syntheses for ceramic materials are described. These syntheses are coprecipitation, molten salts, sol—gel processes, hydrothermal techniques, liquid-phase and gas-phase reactions, polymer pyrolysis, the Pechini and citrate gel methods, aerosols and emulsions. Common themes relating the syntheses are outlined and their advantages over conventional solid-state reactions are described. The scope for further chemical studies on ceramic synthesis is discussed.

Introduction

Worldwide studies on ceramics, polymers and metals during this century have resulted in the establishment of materials science as a scientific discipline. A feature of these studies, particularly for ceramics, is their interdisciplinary nature and at the present time chemistry is making an increasingly important contribution¹ to the research, development and manufacture of ceramic materials. Chemistry has two major roles when applied to ceramics. The first is the synthesis of novel materials, usually in the form of powders. For example, the discovery in 1986 of high-temperature superconductors such YBa₂Cu₃O_{7-x} highlighted the role of chemical synthesis in the preparation of novel ceramics. However, successful exploitation of ceramics requires not only methods for their synthesis but also techniques for their fabrication into useful shapes, e.g., coatings, fibres, monolithic ceramics and powders with a controlled particle size for a wide variety of applications. These applications include controlled-porosity coatings for ceramic membranes, coatings on window glass for selective transmission and reflection of solar radiation, optical fibres and fibres for lightweight thermal insulation, ceramic honeycombs for use in automotive catalytic converters and unaggregated powders for high-strength structural ceramic components.

The second chemical role is in the development of fabrication techniques for ceramic shapes, for example coatings, monoliths and fibres. Synthesis and fabrication fall within the subject area of ceramic processing that occupies an interface between conventional studies in chemistry and materials science. Processing is presently an important feature of ceramic studies in universities and industrial environments while chemical methods for ceramic synthesis are under intense and increasing investigation. This is because, compared to conventional ceramic powder processing² using solid-state reactions between powder reactants, these methods have the potential to yield ceramics with tailored properties and with performance advantages over conventional materials. In this article the conventional method for the preparation of ceramic powders is first described together with the advantages and disadvantages of the technique. The materials requirements for improved ceramics are then outlined. A selection of chemical routes for the synthesis of ceramic materials in the form of powders, coatings, fibres and monoliths are then described together with examples of the syntheses. The chemical principles involved are highlighted along with areas where a greater chemical understanding is required in order to exploit fully the application of chemistry to the processing of ceramic materials.

Conventional synthesis of ceramic powders

The conventional synthesis² for multicomponent ceramic powders is solid-state reaction between oxide and/or carbonate precursors. Thus for barium titanate, BaCO₃ and TiO₂ powders are mixed, milled and calcined. Repeated cycles of milling and calcination are carried out to achieve the solid-state reaction. Relatively high temperatures are required for solid-state reactions, typically around 1200 °C because of limited diffusion during calcination, and this can result in decomposition of the ceramic product. For example the phosphor host material³ GdAl₂B₄O_{10.5} is unstable above 1050 °C and conventional synthesis using oxide powders yielded <5% of the product phase at 1000 °C and only 15-30% at the same temperature after pelletising the oxide reactants. Other disadvantages of the method are the formation of undesirable phases such as BaTi₂O₅ during the preparation of BaTiO₃, large grain sizes (detrimental for high-strength ceramic components) due to firing at high temperature and poor chemical homogeneity particularly when dopant oxides are introduced in small amounts during the synthesis of electroceramics. In addition, particle size reduction by milling can introduce chemical impurities into the ceramic product. Carefully controlled addition of dopants is important in ceramic synthesis. For example, in the preparation⁴ of BaTiO₃-based Y5V and Z5U dielectric compositions for use as multilayer ceramic capacitors, additives include CaZrO3 and CaSnO3 to reduce the Curie point from 130 °C to around 10 °C, MgZrO₃ and CaTiO₃ to smooth out the temperature variation of capacitance as well as modifiers such as CeO₂ and Nb₂O₅ as grain-growth inhibitors. However, the advantages of solid-state reactions are the ready availability of oxide precursors and the low cost for powder production on the industrial scale. These reactions are also convenient for laboratory-scale preparations.

For non-oxide powders, conventional syntheses include the direct reaction of a metal with a gas, e.g., TiN is produced⁵ by nitridation of Ti metal in N_2 at $1500\,^{\circ}\text{C}$. Carbothermal reduction is also a conventional preparation route^{5,6} for nonoxides. Thus TiB₂ is prepared by the carbothermal reduction of a mixture of TiO₂ and B₂O₃ at 1000 °C or by reduction⁶ of TiO₂ with boron carbide and carbon at 2000 °C, while industrial SiC powder is made⁷ in the Acheson process by carbothermal reduction of silica at temperatures higher than 1800 °C. The main disadvantage of conventional syntheses for these refractory non-oxides is the requirement for extensive grinding for particle size reduction, for example to around $0.5-1.0\,\mu m$ for TiN, that introduces chemical impurities into the powders. Precipitation from solution is also a conventional preparation for one-component oxides. In the Bayer process⁸ for manufacture of α-Al₂O₃, bauxite is hydrothermally dissolved in sodium hydroxide to form sodium aluminate solution. An aggregated gibbsite (α-Al₂O₃·3H₂O) powder is produced by seeding the solution with gibbsite crystals and it is converted to α-Al₂O₃ at around 1500 °C although this temperature can be lowered

by the use of fluorine compounds as mineralisers that also modify the shape of α -Al₂O₃ crystals.

Conventional syntheses produce powders which are not particularly suited for the fabrication of coatings and fibres. Chemical routes are attracting attention for ceramic synthesis because some of them allow direct fabrication of coatings, fibres and monoliths without powder intermediates. These routes have the potential to achieve improved chemical homogeneity on the molecular scale which is very important for electroceramics whose electrical functions are determined by the addition of small amounts of dopant oxides. For structural ceramics, improved mechanical properties such as strength can be obtained by removal of powder aggregates and chemical syntheses allow preparation of unaggregated powders. In addition, when chemical routes are used diffusion distances are reduced on calcination compared to conventional preparations owing to mixing of components on the colloidal or molecular level that favours lower crystallisation temperatures for multicomponent ceramics. These potential advantages for improving the performance of ceramic components have given rise to the increased application of chemistry, through ceramic processing, for the development of ceramic materials.

Coprecipitation

The aim in coprecipitation is to prepare multicomponent ceramic oxides through formation of intermediate precipitates, usually hydrous oxides or oxalates, so that an intimate mixture of components is formed during precipitation, and chemical homogeneity is maintained on calcination. This method has been applied to BaTiO₃ powder with a view to fabrication of improved multilayer capacitors. Thus a barium titanyl oxalate precipitate was produced⁹ on addition of oxalic acid to a mixed barium and titanyl chloride solution under controlled conditions of pH, temperature and reactant concentration.

$$BaCl2 + TiOCl2 + 2H2C2O4 + 4H2O \rightarrow$$

$$BaTiO(C2O4), \cdot 4H2O + 4HCl$$
(1)

Dopants such as lanthanides were introduced by coprecipitation and the precipitate was calcined up to 700 °C after collection by filtration, washing and drying to produce a BaTiO₃ powder after milling of 0.4–1.0 μm. In coprecipitation careful control of solution conditions is required to precipitate all cations and thus maintain chemical homogeneity on the molecular scale. Other examples of powders made by coprecipitation are $\text{LiNi}_x\text{Co}_{1-x}\text{O}_2$ with 0 < x < 1 for evaluation¹⁰ as cathode materials in rechargeable lithium-based batteries and nanocrystalline¹¹ yttria-stabilised zirconia (particle size <100 nm) suitable for compaction and sintering to a nanostructured ceramic where the grain size is less than 100 nm. This fine-grained ceramic with potential improved mechanical properties due to the increased percentage of atoms in the grain boundary region cannot be obtained by conventional synthesis owing to the high reaction temperature. The method is also used for the manufacture of high-performance ceramic powders; thus unaggregated Y2O3-stabilised ZrO2 (Tosoh Corporation) with a particle size of around 0.1 µm is produced by coprecipitation of hydroxides from mixed yttrium and zirconyl chloride solutions after which the hydroxide precipitate is dried, calcined and milled. Washing and drying procedures (e.g. water-washing, solvent-washing, azeotropic distillation) that are used for coprecipitated hydroxides can have a drastic effect on the mechanical properties of a sintered powder as they affect the degree of powder aggregation and need to be considered when developing a coprecipitation route to a ceramic powder. Another precipitation technique, not as widely reported as coprecipitation, involves the use of molten salts.

Table 1 Melting points for alkali metal nitrates and eutectic mixtures¹²

metal nitrate	melting point/ $^{\circ}$ C
LiNO ₃	255
NaNO ₃	307
KNO ₃	334
50 mol% NaNO ₃ -50 mol% KNO ₃	220
43 mol% LiNO ₃ -57 mol% KNO ₃	132

Reactions in molten salts

The term molten salt refers¹² to the liquid state of compounds which melt to give liquids displaying a degree of ionic properties. Alkali metal nitrates have relatively low melting points (Table 1) whereas even lower melting points are obtained in their eutectic mixtures. A molten salt can behave as a solvent or as a reactant. Thus in a nitrate melt acid-base reactions can occur according to the Lux-Flood formalism¹³ whereby an acid is an oxide ion acceptor and a base is an oxide ion donor; nitrate ions are bases in this formalism. Nitrite melts are more basic than nitrate melts whereas addition of Lux-Flood bases such as Na₂O₂, Na₂O and NaOH to a nitrate melt increases its basicity. The starting materials for reactions in molten salts are inorganic compounds, in particular sulfates and chlorides, that are blended with the alkali metal nitrates or nitrites as a powder mixture before heating to the reaction temperature. Thus when $Zr(SO_4)_2$ is used, the Zr^{4+} ions formed on dissolution of the zirconium salt in the melt behave as acids according to the Lux-Flood formalism.

Early studies on the synthesis of ZrO₂ investigated¹⁴ the reaction of molten Zr(SO₄)₂ in a LiNO₃–KNO₃ eutectic and ZrO₂ powder was produced for reaction temperatures up to 430 °C. For more basic melts made by additions of Na₂O₂, Na₂O and NaOH, the conversion to ZrO₂ occurred at lower temperatures but favoured formation of alkaline zirconates, although the powder characteristics were not determined. In later work^{15,16} Zr(SO₄)₂ was reacted in a nitrite eutectic of 65 mol% NaNO₂–35 mol% KNO₂ (melting point 220 °C) in a one-stage reaction at 270 °C according to the stoichiometric equation

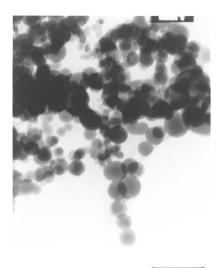
$$Zr(SO_4)_2 + 6NO_2^- \rightarrow ZrO_2 + 2SO_4^{2-} + 2NO_3^- + 4NO$$
 (2)

Tetragonal ZrO₂ (t-ZrO₂) was obtained at 450 °C with a mixture of amorphous and poorly crystalline ZrO₂ at 300 °C which crystallised to t-ZrO2 at 500 °C; ZrO2 had a crystallite size of 5 nm and specific surface area greater than 150 m² g⁻¹. Reaction of Zr(OCl)₂ with a NaNO₃-KNO₃ eutectic at 250 °C yielded¹⁷ amorphous ZrO₂ which crystallised to tetragonal ZrO₂ on calcination, although the conversion temperature for the tetragonal phase decreased as the reaction temperature increased and it was produced directly at 450 °C. For 3 mol% Y₂O₃-ZrO₂ the reaction¹⁸ was carried out at 450 °C between Zr(OCl)₂ and YCl₃ in a NaNO₃-KNO₃ eutectic. The reaction product, $t\text{-}ZrO_2$ powder, which had specific surface areas around 110 m² g⁻¹ and a crystallite size of 6–10 nm, could be pressed and sintered at 1500 °C to 98.5% of the theoretical density, although the extent of powder aggregation was sensitive to washing and drying procedures. Alumina-zirconia solid solutions have also been produced¹⁹ in powder form from Zr(OCl)₂ and AlCl₃ in a NaNO₃–KNO₃ eutectic, and reactions in molten salts have not been restricted to zirconia-based systems. In a recent study 20 cubic $Ba_{0.75}Sr_{0.25}TiO_2$ was prepared by the addition of a BaCO₃-SrCO₃-TiO₂ mixture to a eutectic melt of 49 mol% NaOH-51 mol% KOH at 300°C for 12 h. For this reaction the eutectic was a solvent in which the reaction kinetics were considerably faster than in the conventional solid-state reaction.

Reactions in molten salts can be considered to fall within the general class of reactions in non-aqueous liquids and have not been widely applied for ceramic powder preparation even though the reactants are readily available. The nucleation, growth and aggregation of ceramic powders during preparation is of fundamental importance to the usefulness of the powders and is an area of continuing debate within activities in ceramic processing. If unaggregated powders can be obtained in melts for a wide range of compositions then molten salt chemistry could, in the future, offer an attractive route for synthesis of ceramic powders.

Sol-gel processing of colloids

Colloid science is important for the successful application of chemistry to ceramic synthesis. This is because powder preparation involves nucleation and growth of particles to a size often less than 1 µm and thus the powders are colloidal systems.21 In addition powders are often handled in the form of colloidal dispersions and this is illustrated by the synthesis method known as sol-gel processing of colloids. A sol-gel preparation can be divided7 into five stages. The starting material, for example a metal salt, is converted in a chemical process to a dispersible oxide, which forms a colloidal dispersion (sol) on addition to dilute acid or H₂O. Removal of H₂O and/or anions from the sol produces a stiff gel in the form of spheres, fibres, fragments or coatings and this transition is usually reversible. Calcination of the gel in air yields an oxide product after decomposition of the salts. For example, ceria sols have been made⁷ by first adding NH₃(aq)-H₂O₂ to cerium(III) nitrate solution. After careful washing of the CeIV hydrate to remove entrained electrolyte the precipitate was peptised with HNO₃ to sols with a particle size of around 8 nm. While peptisation involves breaking up coarse precipitates, deanionisation of metal salt solutions involves growing molecular species to colloidal units in the form of polynuclear ions. For example, treatment²² of chromium(III) nitrate solution with a long-chain primary amine removes hydrolytic HNO₃ from the aqueous solution with the resultant formation of polymeric colloidal species. Flame-hydrolysed powders²³ such as SiO₂ also form sols on dispersion in water. An example of a sol is shown in Fig. 1. It is useful to note that many of the chemical techniques attracting attention for ceramic synthesis are not new and often date back many years. Thus sol-gel processing of colloids was first exploited in the late 1950s for fabrication of ThO₂-UO₂ ceramics for use⁷ as spherical fuel powders in high-temperature thermal nuclear reactors. For preparation of multicomponent oxides, sols are blended together before gelation and a component unavailable in sol



200nm

Fig. 1 Transmission electron micrograph of a silica sol

form can be introduced as an electrolyte solution or oxide powder. Spherical sol-gel powders can be made by the following processes.

- (1) Dispersing a sol to an emulsion in an immiscible organic solvent capable of extracting H_2O from the sol, for example 2-ethylhexanol. Gelation occurs during the dehydration process and this approach was used for thoria-based nuclear fuels.
- (2) External gelation in which a sol is dispersed to an emulsion in a water-immiscible solvent and gelation is effected by addition of a long-chain amine or $NH_3(g)$ to the solvent.
- (3) Internal gelation in which an ammonia donor such as hexamethylenetetramine or urea is added to the sol before emulsification and gelation occurs by release of NH₃(g) on warming solvent.

Spray-drying²⁴ sols also produces spherical powders. Examples^{1,7} of sol–gel powders are electrically conducting ceramics such as Ni_{0.3}Zn_{0.7}Fe₂O₄ and 3% SnO₂–In₂O₃, plasma-spray Cr₂O₃–ZrO₂ powders around 10 μm diameter and catalyst supports. Advantages of this sol–gel technique are good chemical homogeneity due to mixing components at the colloidal level and lower reaction temperatures; thus high-density ThO₂–UO₂ spheres were obtained at 1150 °C, considerably lower than for the conventional powder mixing method (*ca.* 1700 °C). In addition, because it involves handling liquid feeds, small amounts of dopants can be readily introduced while lower crystallisation temperatures enable preparation of phases that are unstable at high temperature.

The versatility of sol-gel processing is illustrated by its use for fabrication of ceramic shapes other than powders. Thus thin oxide coatings around 1 µm can be prepared⁷ on substrates by first applying a sol by spinning or dip-coating after which the liquid layer is dried to a gel coating that is calcined to oxide. As an example, 25 silica coatings for improved oxidation resistance of stainless-steel wire mesh were prepared by dipcoating. Although the technique is low cost and simple to carry out, cracking and loss of adhesion can occur on drying. Fibres can be drawn^{26,27} from sols with controlled rheological properties and calcined to oxide. Whereas aluminosilicate fibres are conventionally prepared from a melt which limits the Al₂O₃ content to around 65 mass% owing to the melt viscosity, the use of sol-gel yields a much wider range of compositions such as 95% Al₂O₃-5% SiO₂ and a range of polycrystalline ceramic fibres are manufactured²⁷ from sol-gel materials. Preparation of sol-gel fibres is an example of powderless processing that avoids the synthesis of a ceramic powder with a well defined particle size and its subsequent consolidation into a shape. Powderless processing is an attractive method for fabrication of ceramic monoliths as it can produce near-net size and shape components in a few processing steps. For example, SiO₂ sols in combination with potassium silicate and a hydrolytic agent such as formamide were cast^{28,29} directly to monolithic silica gels with a controlled pore size in the range 100-300 nm. After leaching out K + ions, the gels were dried by using microwaves and sintered to silica monoliths. A key feature of the synthesis was that large pore sizes reduced the capillary forces on drying the gel, thus preventing cracks in the ceramic. Powderless processing also includes freeze casting.³⁰ For example, SiO₂ sols were cast into a mould, frozen in liquid nitrogen and the mould was then removed. After thawing, the intact gel was calcined to a nearnet size and shape component. An important aspect of these fabrication processes is colloidal processing31 in which the tendency of sol particles to flocculate and coagulate with the resultant effect on porosity is controlled, but a greater understanding of changes in sol structure taking place during fabrication is required to fully utilise these powderless processing techniques for a wide range of oxide ceramics.

The hydrolysis of cations^{32–34} and inorganic polymerisation in aqueous solution are of fundamental importance to wet chemical methods of synthesis such as sol–gel in which sols

are formed from cations that can undergo hydrolysis. Monovalent hydrolysis products whose formation¹ is represented by the equation

$$[M(H_2O)_n]^{z+} \rightarrow [M(OH)_p(H_2O)_{n-p}]^{(z-p)+} + pH^+$$
 (3)

where n is the number of bound water molecules, p is the number of protons removed from the cation on hydrolysis and z is the valency of the cation M, can condense to polyvalent or polynuclear ions which can be colloidal, for example, $[AlO_4Al_{12}(OH)_{25}(H_2O)_{11}]^{6+}$; polynuclear ions contain OH bridges, M-OH-M (olation) or oxygen bridges, M-O-M (oxolation) and are precursors for particle growth. A quantitative approach for predicting the products of cation hydrolysis as a function of the experimental conditions, known as the partial charge model, 33,34 has been developed. In this thermodynamic model, proton exchange (and the associated electron transfer) between metal ions and solution occurs until the mean electronegativity of the hydrolysed species becomes equal to the mean electronegativity of the surrounding aqueous solution. The ability to predict solution species and their condensation behaviour is a very useful tool for understanding the chemistry of sol-gel processes.

Sol-gel processing of metal-organic compounds

The phrase sol-gel has been used inaccurately in the scientific literature and is often assigned to all wet chemical methods for ceramic synthesis even though there are only two sol-gel processing techniques. The second³⁵ sol-gel technique involves ceramic synthesis by hydrolysis of metal-organic compounds, in particular metal alkoxides,36 M(OR)z where R is an alkyl group, and at the present time publications on sol-gel dominate the literature on ceramic synthesis. This method is particularly associated with non-fusion routes to oxide glasses. For preparation of multicomponent oxides, alkoxides are mixed together in alcohol and a component unavailable as an alkoxide is introduced as a salt, for example an acetate, so that the resulting solution has the required ceramic composition. Hydrolysis is carried out under controlled conditions of pH, added H₂O, alkoxide and alcohol concentration. The reaction conditions can result in the solution forming a solid monolithic gel (known as an alcogel) which is dried and calcined to an oxide powder, or precipitation of powders directly from solution. The reactions occurring in solution are complex³² but involve hydrolysis and condensation to polymeric species as represented by the equations

$$M(OR)_z + H_2O \rightarrow M(OR)_{z-1}(OH) + ROH$$
 (4)

$$2M(OR)_{z-1}(OH) \rightarrow M_2O(OR)_{2z-2} + H_2O$$
 (5)

$$M(OR)_z + M(OR)_{z-1}(OH) \rightarrow M_2O(OR)_{2z-2} + ROH$$
 (6)

Metal-oxygen-metal (M-O-M) bonds are formed in solution by self-condensation or by cross-condensation when different alkoxides are used, thus M'-O-M. Sol-gel processing with alkoxides shares the same versatility and benefits as the use of colloids but has some additional advantages. Because many alkoxides are liquids or volatile solids they can be purified to form extremely pure oxide sources which is important for electroceramic synthesis, while improved chemical homogeneity is obtained owing to mixing of components at the molecular level. The improved homogeneity is associated with lower crystallisation temperatures than for use of colloids, often between 400 and 800 °C for gel→oxide conversion. However, alkoxides are relatively expensive compared to precursors for sol-gel processing of colloids, a limited range of them are commercially available and their use involves a solvent-based rather than a water-based process. There are certainly requirements³⁷ to develop economical syntheses for large quantities of alkoxides to fully exploit the process. Many chemical studies have been carried out on characterising

alkoxide solutions in order to relate the solution properties of the precursors to the ceramic properties. Techniques³⁵ have included light scattering, small-angle X-ray scattering, NMR spectroscopy, liquid chromatography and this characterisation is an active area of sol–gel studies. As for all chemical syntheses the success of a sol–gel synthesis is ultimately judged by the performance of the chemically derived ceramic.

Sol-gel processing of metal alkoxides has been widely used for the preparation of submicrometre oxide powders. For example, $Y_3Fe_5O_{12}$ was prepared³⁸ by hydrolysis of a mixture of $Fe(OC_2H_5)_3$ in C_2H_5OH and $Y(OC_4H_9)_3$ in xylene. The resulting gel was, after drying, converted at 700 °C to Y₃Fe₅O₁₂ with a mean diameter of 9 nm. Alkoxides have differing hydrolysis rates and the benefits of improved homogeneity can thus be lost during hydrolysis of mixed alkoxides. Modification of hydrolysis rates which affect particle formation, growth and aggregation can be made by complexing the alkoxide with a chelating ligand. For example, Zr(OC₃H₇)₄ can be complexed with acetylacetone and hydrolysis of this alkoxide with³⁹ toluene-p-sulfonic acid in the presence of acetylacetone yielded ZrO₂ particles around 3 nm in diameter after ageing the reactants at 60 °C. Monodispersed spherical powders, usually submicrometre, can be obtained by controlled hydrolysis of alkoxide solutions and are known as Stöber spheres. 40,41 An example of a powder made by controlled hydrolysis (also known as homogeneous nucleation) is shown in Fig. 2 and the mechanism of particle formation and growth is of relevance to other ceramic syntheses. While powder formation by homogeneous nucleation has often been considered to involve nucleation from supersaturated solutions at a critical particle size followed by diffusion of molecular species onto growing nuclei, recent studies⁴²⁻⁴⁴ suggest an alternative mechanism in which nucleation followed by aggregation of small particles takes place during particle growth.

Many electroceramics are used in the form of thin coatings, around 1 µm, and the development of sol-gel coatings is an area of expanding activity; a sol-gel PbTiO3 coating is shown in Fig. 3. Alkoxide-derived coatings include Pb_{1-x}La_{2x/3}TiO₃ where x is between 0 and 0.2 for pyroelectric applications, ⁴⁵ and La_{0.5}Sr_{0.5}CoO₃ electrode materials⁴⁶ while the ability of chemical methods to tailor the properties of ceramics is highlighted by fabrication of ceramic membranes. 47-49 While polymer membranes are widely available, ceramic membranes have operating advantages, in particular superior chemical and thermal durabilities. Nanofiltration membranes have pore diameters in the separation layer around 2 nm and have been prepared⁴⁸ by controlled hydrolysis of Zr(OC₅H₁₁)₄ to ZrO₂ particles less than 5 nm in diameter. These particles were then deposited from a dispersion onto a substrate to produce the membrane layer. Alcogels can be dried and sintered to crack-

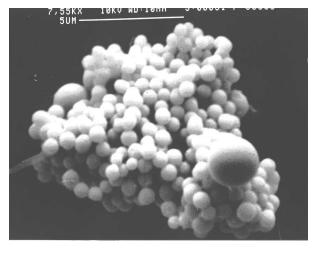


Fig. 2 Titania spheres by controlled hydrolysis of an alkoxide



Fig. 3 Sol-gel lead titanate coating

free monolithic components. Silica alcogels were prepared⁵⁰ from hydrolysed Si(OC₂H₅)₄ solutions in the presence of a drying control chemical additive, formamide, which modified the pore size distribution in the alcogel producing an average pore size around 5 nm. This modification allowed conversion of the alcogel to crack-free silica components. Alcogels can also be converted by supercritical drying to aerogels^{51,52} which are transparent, porous solids with high surface area and densities as low as 0.003 g cm⁻³. In supercritical drying, pore fluid is removed directly above its critical point. For C₂H₅OH, the common solvent in sol-gel processing, the critical temperature and pressure are 243 °C and 6.4 MPa respectively, but recently a low-temperature method has been introduced⁵² in which ethanol is replaced by CO₂ and the latter is removed above its critical point, 31 °C and 7.2 MPa; the lower critical temperature is a processing advantage.

Ceramics are hard, brittle solids whereas polymers are tough, flexible and ductile. Hybrid polymer-ceramic materials can share the advantages of these two types of materials while minimising the disadvantages. These materials have been called ceramers⁵³ to indicate a material that has a unique combination of ceramic and polymer properties, ormosils⁵⁴ which refers specifically to an organically modified silicate for a SiO₂-based system but are now more generally known as ormocers⁵⁵ (organically modified ceramics). Alkoxides have a central role in the synthesis of ormocers. While the use of alkoxides for oxide synthesis involves precursors where all attached alkoxy groups can be replaced on hydrolysis, preparation of ormocers uses precursors in which some attached groups are retained on reaction. These hybrid materials contain an inorganic backbone and organic components that produce chemical or structural modification of the inorganic network. Low-temperature curing (ca. 150 °C) produces the ormocer solid in contrast with high crystallisation temperatures required for oxide ceramics. As an example, an ormocer was prepared⁵⁴ by reaction of a silanol-terminated polydimethylsiloxane (molecular mass 1750) with acidified Si(OC₂H₅)₄ at 80 °C and gelation occurred at ambient temperature. Potential applications of ormocers are many,56 including optoelectronics, sensors, coatings, elastomers and porous materials. Development of ormocers is an exciting area of materials science where there is considerable scope for innovative sol-gel chemistry to produce novel materials with tailored properties.

Hydrothermal synthesis

Hydrothermal techniques are widely used in industrial processes for the dissolution of bauxite prior to precipitation of gibbsite in the Bayer process and for the preparation of aluminosilicate zeolites. Interest in this method for synthesis

of ceramic powders, as measured by the number of publications, is much less than in the two sol-gel processes. This is surprising because hydrothermal synthesis offers a low-temperature, direct route to submicrometre, oxide powders with a narrow size distribution avoiding the calcination step required in sol-gel processing. When applied to ceramic powders hydrothermal techniques often involve heating metal salts, oxides or hydroxides as a solution or suspension in a liquid at elevated temperature and pressure up to about 300 °C and 100 MPa. Syntheses that offer a lower temperature route⁵⁷ than solidstate reactions to compounds are frequently described as soft chemistry routes or chimie douce reactions, although these terms have not been widely used in the ceramic literature. The advantage of hydrothermal synthesis is illustrated by the preparation of BaFe₁₂O₁₉⁵⁸ from a suspension of Ba(OH)₂ and α-FeOOH. Single-phase submicrometre ferrite particles were obtained at 325 °C compared with a temperature between 1150 and 1250 °C in the conventional solid-state synthesis by firing a mixture of α-Fe₂O₃ and BaCO₃. For SrFe₁₂O₁₉, coprecipitated mixed strontium(II) and iron(III) hydroxides were heated in the temperature range 160-220 °C for up to 5 h, yielding strontium hexaferrite⁵⁹ powder, about $2 \mu m$ in diameter with a platelet morphology. This reaction temperature is low compared to 1250 °C for the conventional solid-state reaction between SrCO₃ and Fe₂O₃ and 800 °C for coprecipitation. The hydrolysis reaction represented in eqn. (3) can become more pronounced under hydrothermal conditions compared to ambient temperatures leading to direct formation of oxide powders from electrolyte solutions. This type of reaction is known as forced hydrolysis. As an example, monoclinic ZrO₂ powder with particle diameters in the range 1-10 nm was produced⁶⁰ by heating a 0.2 mol dm⁻³ solution of ZrO(NO₃)₂ at pH 0.5. Hydrothermal techniques have also been used for fabrication of thin films, for example $\mathrm{BaTiO_3}^{61}$ on Ti substrates.

Understanding the reaction mechanism of hydrothermal syntheses and the nature of solution species can help in the production of powders with well defined properties. Dissolution-recrystallisation processes are considered important in particle nucleation and growth under hydrothermal conditions while polynuclear ions that are precursors for sol-gel processes are important for forced hydrolysis reactions. For example a tetrameric species [Zr(OH)₂·4H₂O]₄⁸⁺ has been considered⁶⁰ to form particles of critical size which nucleated from solution and grew by aggregation. Thermodynamic modelling of hydrothermal processes has been carried out, particularly for BaTiO3,62 and these calculations indicate the stability of the desired product under different conditions, namely pH, temperature and reagent concentrations. Although many chemical syntheses are very different from a practical viewpoint, they are often related by underlying chemical themes. Hence a greater knowledge of the formation and structure of solution species will be useful in increasing understanding of powder formation in sol-gel and hydrothermal processes.

Polymer pyrolysis

Polymer pyrolysis refers to the synthesis of a polymeric compound, sometimes called a preceramic polymer, which is then fabricated into a shape and pyrolysed to the ceramic. Polymer pyrolysis is particularly associated with the synthesis of high-tensile strength β-SiC fibre as a result of pioneering work 63,64 carried out in the 1970s. This work involved thermal rearrangement of polysilanes to polycarbosilanes. For example, $(CH_3)_2SiCl_2$ was converted by reaction with Li to dodecamethylcyclohexasilane, $[(CH_3)_2Si]_6$ which underwent ring-opening and polymerisation at $400\,^{\circ}C$ under Ar to yield a polycarbosilane. Continuous polycarbosilane fibre could be prepared either by drawing from solution or by melt-spinning and was pyrolysed to β-SiC fibres although the molecular

mass distribution of the polycarbosilane affected the fibre quality. These studies also led to a process for the manufacture⁷ of continuous polycrystalline β-SiC fibre and an important step in the process is curing of polycarbosilane fibres in O₂ which cross-links molecular chains of the polymer preventing melting during polymer decomposition. Conversion of polycarbosilanes to fibre is a further example of powderless processing. Besides their use in the preparation of fibres, preceramic polymers can be applied as films and moulded into shapes that can be cured and pyrolysed to near net-shape ceramic components with high purity and compositional homogeneity at relatively low temperature. They are also used to build-up the matrix, by impregnation, of fibre-reinforced ceramic matrix composites. These benefits for fabrication have led to increased interest in the chemical design of preceramic polymers that can be converted directly to ceramic fibres and monoliths. Another preceramic polymer is polysilastyrene,66 a soluble phenylmethylpolysilane made by reaction of (CH₃)₂SiCl₂ and C₆H₅CH₃SiCl₂ with Na in toluene. Solubility, melting point, the curing process (whether by heat treatment or by ultraviolet irradiation) and, in particular, ceramic yield on pyrolysis are all important properties for successful use of preceramic polymers, and further examples of the range of materials developed are shown⁶⁷ in Table 2. This area of ceramics where synthesis has a crucial role is under increasing^{68,69} investigation.

Polymer pyrolysis is not restricted to Si-based systems. Thus, reaction of B₁₀H₁₄ with diamines such as NH₂CH₂CH₂NH₂ yielded a solid preceramic polymer⁷⁰ which was pyrolysed in NH₃ at 1000 °C to a BN-containing powder. For AlN, anodic dissolution of Al in acetonitrile containing a primary amine and a tetraalkylammonium salt (for increasing the solution conductivity) produced⁷¹ a liquid with composition Al(NHR)₃ that underwent polymerisation to a solid gel with composition Al₂(NR)₃. The latter was pyrolysed above 800 °C in NH₃ to AlN powder with a crystallite size of 25 nm. Although this last example involves polymer pyrolysis it can also be classified as a non-aqueous liquid-phase reaction.

Non-aqueous liquid-phase reactions

Liquid-phase reactions take place in a non-aqueous solvent, which may be inert or one of the reactants, and are associated with the synthesis of non-oxide powders, particularly Si₃N₄. An interfacial reaction^{7,72} occurs between SiCl₄(1) in a mixed cyclohexane-benzene solvent and NH₃(1) at -40 °C producing an amorphous solid, silicon diimide Si(NH)2, which decomposes on heating to 1400 °C to α-Si₃N₄. This reaction forms the basis for a commercial route to Si₃N₄ powder (Ube Industries) which consists of equiaxed particles, about $0.1-0.2 \,\mu m$ in size, containing 95% of the α -phase and 5% of β-Si₃N₄; this powder contains lower levels of impurities than those from other syntheses for Si₃N₄ such as solid-state reaction, as the reactants can be readily purified. Other metallic nitrides have been⁷³ made by similar interfacial reactions, for

Table 2 Ceramic product and yield from preceramic polymers⁶⁷

precursor	temperature/°C; atmosphere	product	yield (mass%)
polymethylvinylsilane	1000; Ar	SiC	83
polytitanocarbosilane	1300; N ₂	$SiC_xO_vTi_w$	75
polyhydridosilazane	1200; N_2	Si_3N_4	74
polymethylsilazane	800; NH ₃	Si_3N_4	85
polyvinylsilazane	1200; N ₂	SiC_xN_y/C	85
polyvinylphenylsilazane	1000; N ₂	Si_3N_4	85
polycyclomethylsilazane	1000; Ar	Si ₃ N ₄ /SiC	88
polyborosilazane	1000; Ar	BN/Si ₃ N ₄	90
polyboronsiliconimide	1250; NH ₃	SiB_xN_v	72
polymethylsiloxane	1000; He	SiO_xC_y	85
polyphenylsilsesquioxane	1400; Ar	SiC_xO_y	78

example cubic vanadium nitride with a particle size of 0.1-1 µm is formed by decomposition of the product of the reaction of VCl₄(1) and NH₃(1) at 1500 °C in NH₃. For borides, Ti(BH₄)₃, obtained from the reaction⁶ of B₂H₆ with Ti(OC₄H₉)₄, decomposed at 140 °C in xylene according to the equation

$$2\text{Ti}(BH_4)_3 \rightarrow 2\text{Ti}B_2 + B_2H_6 + 9H_2$$
 (7)

to give an aggregated TiB2 powder of high purity with a particle size of 0.1–0.2 μm, while cubic ZnS was obtained⁷⁴ on passing H₂S through a diethylzinc solution at ambient temperature. In an extension of sol-gel processing to non-oxides, amorphous GeS_2 was obtained 75 by reaction of H_2S with Ge(OC₂H₅)₄ at ambient temperature and crystallised on heating, although it was easily contaminated with GeO₂. Lowtemperature decomposition is an advantage of non-aqueous reactions that have been extended to oxides and include condensation between metal chlorides and metal alkoxides, which has been referred⁷⁶ to as a non-hydrolytic sol-gel reaction represented by the equation

$$MCl_z + M(OR)_z \rightarrow Cl_{z-1}MOM(OR)_{z-1} + RCl \rightarrow$$

$$2MO_{z/2} + zRCl$$
(8)

For example, TiCl₄ and Ti(OC₃H₇)₄ were heated together at 110 °C and the resulting monolithic gel was decomposed to anatase at 500 °C. Non-hydrolytic reactions can be carried out by reaction of a metal chloride with an ether⁷⁷ which forms an intermediate adduct and then a metal chloroalkoxide. This approach has a processing advantage as the use of alkoxides, which may be difficult to synthesise, is avoided. For example, $VOCl_3$ was reacted with $(C_3H_7)_2O$ at $110\,^{\circ}C$ and the resulting gel was decomposed at 500 $^{\circ}\text{C}$ to orthorhombic V_2O_5 powder.

Aerosol-derived powders

Two aerosol routes are used for powder preparation. The first involves generation of a supersaturated vapour from a reactant followed by homogeneous nucleation, while the second involves generation of liquid droplets by various methods which undergo a heat treatment to solid particles. For example, 78 the silazane precursor $[CH_3SiHNH]_n$ where n=3 or 4, which was made by ammonolysis of CH3SiHCl2, was decomposed to a vapour at about 1000 °C in NH3. Rapid condensation of the gaseous product produced nanometre-sized ceramic powders in the Si(N,C) system. Liquid droplets can be generated by use of pneumatic jet atomisation or ultrasonic atomisation after which the droplets are dried and transported by a carrier gas to a furnace where they are decomposed to oxide powders. Decomposition of droplets in this way is often referred⁷⁹ to as spray-pyrolysis. Compared to conventional powder synthesis, aerosol methods have the ability to produce spherical particles with sizes ranging from micrometres down to 100 nm with high purity and chemical homogeneity for complex metal oxides. An example⁸⁰ of an aerosol-derived cathodoluminescent phosphor, Y_{2.82}Tb_{0.18}Ga_{2.5}Al_{2.5}O₁₂, made by ultrasonic atomisation is shown in Fig. 4. Other materials made by aerosol methods include submicrometre SrFe₁₂O₁₉,81 while electrostatic atomisation has been used for synthesis of ZrO₂ powder.82

Spray-drying²⁴ is used in industrial processes for converting a liquid feed into a dry powder. When applied to ceramic powders the feed can consist of oxide colloids or salt solutions and when these precursors are used spray-drying is analogous to aerosol techniques. Spray-dried powders are often larger than aerosol-derived powders, around 10 µm in diameter. This technique is a convenient way to prepare multicomponent oxides with good chemical homogeneity. For example, GdAl₂B₄O_{10.5}, which could not be obtained³ in high yield by solid-state reactions between oxides owing to its decomposition above 1050 °C, was readily prepared as a single phase by

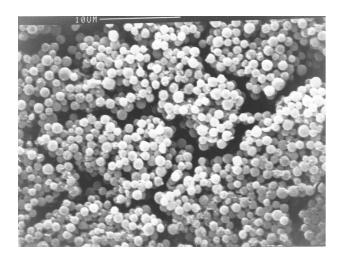


Fig. 4 Aerosol-derived $Y_{2.82}Tb_{0.18}Ga_{2.5}Al_{2.5}O_{12}$ powder

spray-drying mixed electrolyte solutions followed by calcination at 950 $^{\circ}$ C. Spray-roasting or spray-calcination involves converting a liquid feed to droplets that are fed directly to a furnace and powder sizes obtained from this technique and spray-drying are similar. Spray-roasting has been used to manufacture⁸³ multicomponent ceramics, for example ferrites such as MnFe₂O₄.

Gas-phase reactions

Reactions between gases have been used to prepare both oxides and non-oxide powders on the laboratory and industrial scale. These reactions are characterised by the use of a variety of heating techniques including furnace heating, lasers, gas plasmas and flame propagation, while the underlying chemical principle that determines particle formation is homogeneous nucleation from supersaturated vapours. In flame-hydrolysis,84 volatile compounds such as SiCl₄ are passed through an oxygen-hydrogen stationary flame. Molten primary oxide particles formed by nucleation grow by coalescence to larger droplets. As particles solidify they stick together on collision, forming solid aggregates which then associate to loosely bound agglomerates. Flame-hydrolysed silicas have been used²³ in sol-gel processing while examples of other flame-hydrolysed oxides are shown in Table 3. Pioneering work⁸⁵ on the use of high-powered lasers to heat gases yielded Si₃N₄ with a particle size between 10 and 25 nm and nitrogen surface area of 117 m² g⁻¹ from a mixture of SiH₄ and NH₃. Silane has a strong absorbance band at 10.6 µm, near the wavelength of CO₂ lasers, and was decomposed to a supersaturated Si vapour which reacted with NH₃. These reactions are characterised by fast heating and cooling rates (106 K s⁻¹ and 105 K s⁻¹ respectively) and reaction times around 10^{-3} s. Different precursors have been used in laser-driven reactions; for example, 86 mixed Si₃N₄-SiC powders with an average particle size of

Table 3 Oxides made by flame hydrolysis⁸⁴

oxide	raw material	boiling point/°C
SiO ₂	SiCl ₄	57
$Al_2\tilde{O}_3$	AlCl ₃	180^{a}
TiŌ,	TiCl ₄	137
Cr ₂ O ₃	CrO ₂ Cl ₂	117
Fe ₂ O ₃	$Fe(CO)_5^2$	103
GeO_2	GeCl₄	84
NiO	Ni(CO) ₄	42
SnO_2	SnCl ₄	114
$V_2O_5^2$	VOCl ₃	127
ZrO_2	$ZrCl_4$	331^{a}

^aSublimation temperature.

20 nm were obtained from a mixture of hexamethyldisilazane, (CH₃)₃SiNHSi(CH₃)₃ and NH₃. Direct current argon plasmas have been used to prepare⁸⁷ TiN powders with diameters around 10 nm by heating a mixture of TiCl₄ and NH₃ at 1100 °C. Plasma-derived powders which had a much finer particle size than commercial TiN (size around 0.5–1.0 μm) prepared by nitridation of Ti could be pressureless sintered at 1400 °C whereas the conventional powder is difficult to sinter and requires hot-pressing at temperatures higher than 1800 °C.

Pechini and citrate gel methods

In the Pechini method, 88 polybasic chelates are formed between α-hydroxycarboxylic acids containing at least one hydroxy group, for example citric acid, HOC(CH₂CO₂H)₂·CO₂H with metallic ions. The chelate undergoes polyesterification on heating with a polyfunctional alcohol, for example ethylene glycol, HOCH2CH2OH. Further heating produces a viscous resin, then a rigid transparent, glassy gel and finally a fine oxide powder. Advantages of the Pechini method are the ability to prepare complex compositions, good homogeneity through mixing at the molecular level in solution and control of the stoichiometry. Low firing temperatures are required for decomposition of the resin to the oxide, thus 650 °C for BaTiO₃ compared to 1000 °C for the conventional solid-state reaction. This is a versatile method for the synthesis of multicomponent oxides, for example Pb₃MgNb₂O₉. 89 The citrate gel^{90,91} method shares the advantages of the Pechini method with respect to chemical homogeneity and compositional control. For the synthesis⁹² of YBa₂Cu₃O_{7-x} metal nitrate solutions of Y, Ba and Cu were added to citric acid solution and the pH raised to between 6.5 and 7.0 in order to dissolve insoluble barium citrate but not to precipitate metal hydroxides. The solution, which contained polybasic chelates, was concentrated to a viscous resin and dried to a transparent gel that was pyrolysed to a fine powder. The citrate gel method is also a versatile method for synthesis of multicomponent oxides, for example $SrCo_{0.8}Fe_{0.2}O_{3-x}$. 93

A claimed advantage of many chemical syntheses is their improved homogeneity although evidence for this is not always available. However, a recent study using Raman and ¹³C NMR spectroscopy indicated that during the preparation ⁹⁴ of BaTiO₃ by the Pechini method the coordination of Ba and Ti in the mixed metal complex remained almost unchanged on polymerisation and that molecular-level mixing was retained at the resin stage and probably in the pyrolysed resin. There is further scope for using characterisation techniques for monitoring changes in homogeneity at different stages of the wide range of chemical syntheses.

Emulsion-derived powders

Emulsions have been used widely in aqueous sol–gel processes for converting sols to gel powders by dehydration, internal gelation and external gelation as was described earlier. Powders made by these methods have sizes in the range of 1 μ m or larger and emulsion methods have been extended to include use of microemulsions, enabling preparation of ceramic particles in the nanometre size range. Thus Fe₃O₄ powders were made⁹⁵ by precipitation from Fe³⁺/Fe²⁺ salts with NH₃ (aq) in microemulsions of sodium bis(2-ethylhexyl)sulfosuccinate (Aerosol OT)–heptane–H₂O while TiO₂ particles with diameters less than 10 nm were prepared⁹⁶ by controlled hydrolysis of Ti(OC₃H₇)₄ in reverse micelles of Aerosol OT produced in an Aerosol OT–hexane–H₂O solution; the TiO₂ nanoparticles aggregated into sols with sizes of 20 to 200 nm, eventually forming gelatinous precipitates.

Conclusions

Studies on ceramics are interdisciplinary and chemistry has an increasingly important role in the research, development and manufacture of these materials. Chemical methods for ceramic synthesis, a selection of which have been described, are also known as soft chemistry routes and offer a lower temperature route to ceramic materials compared to conventional solidstate reactions between oxide powders. They also allow direct fabrication of ceramics as coatings, fibres and monoliths. For the syntheses under discussion, molten salt reactions offer a straightforward route to ceramic powders using readily available precursors, although their extension to a wide range of compositions requires further study. Sol-gel processing with both aqueous oxide colloids and alkoxides has attracted tremendous attention as measured by the numbers of publications. Aqueous sol-gel processing methods avoid the use of organic solvents, which is a practical advantage, and involve low-cost precursors. Full exploitation of the alkoxide route, particularly for powders, requires economical synthesis of metal alkoxides but this method is very useful for fabrication of thin oxide coatings where the cost of the precursor is not a critical factor. A major development of sol-gel processing has been on organic-inorganic hybrids and there is considerable potential here for innovative chemical synthesis of new materials with tailored properties. Other gel methods, the Pechini and citrate gel techniques, have been shown to be very useful for synthesis of multicomponent electroceramic powders.

Sol-gel processing has been applied mainly to oxide ceramics. There is scope for extending sol-gel processing of alkoxides to non-oxide ceramics which links sol-gel to nonaqueous liquid-phase reactions. The latter have been widely applied to non-oxide powders, in particular for the manufacture of silicon nitride. Hydrothermal synthesis and sol-gel processing, although very different from a practical viewpoint, involve hydrolysis of solution species. Increased knowledge about the formation of hydrolysis products in solution would enhance understanding of the processes involved in particle formation from solution. Hydrothermal synthesis is an established industrial process and offers a direct route to oxide powders, but it has not attracted the attention given to sol-gel methods. There is potential for extending hydrothermal methods to a wide range of compositions for both oxide and non-oxide powders. Control of powder aggregation, for example in coprecipitation and molten salt reactions, is important for ceramic applications and needs to be considered when carrying out a synthesis. A key advantage of polymer pyrolysis over other methods is its ability to yield high-strength nonoxide fibres, and there is considerable scope for chemical design of polymers suitable for conversion to fibres, coatings and monolithic ceramics. Chemical methods have the ability to produce powders with an exceptionally small size in the nanometre range; gas-phase reactions, microemulsions and aerosol methods are particularly suited for preparation of nanoparticles. However, the success of chemical syntheses of ceramic materials can be judged primarily by whether they result in improved materials properties and performance. In order to fully exploit chemical methods now and in the next century a close interaction is required between ceramic studies carried out in the disciplines of chemistry and materials science.

References

- D. L. Segal, in Materials Science and Technology: A Comprehensive Treatment. Processing of Ceramics, vol. 17A, ed. R. J. Brook, VCH Publishers, Weinheim, 1996, p. 69.
- A. J. Moulson and J. M. Herbert, Electroceramics: Materials, Properties and Applications, Chapman and Hall, London, 1990,
- H. A. M. van Hal and W. A. Groen, in Proceedings of the Electroceramics IV4th International Conference on Electroceramics

- and Applications, ed. R. Waser, S. Hoffman, D. Bonnenberg and Ch. Hoffman, Verlag der Augustinus Buchhandlung, Aachen, 1994, p. 1339.
- M. S. H. Chu and A. W. J. M. Rae, in Ceramic Transactions, volume 49: Manufacture of Ceramic Components, ed. B. Hiremath, A. Bruce and A. Ghosh, The American Ceramic Society, Westerville, OH,
- A. Jones, in Ceramic Technology International 1993, ed. I. Birkby, Sterling Publications Limited, Hong Kong, 1992, p. 71.
- M. K. Gallagher, W. E. Rhine and H. K. Bowen, in Ultrastructure Processing of Advanced Ceramics, ed. J. D. Mackenzie and D. R. Ulrich, Wiley, New York, 1988, p. 901.
- D. L. Segal, Chemical Synthesis of Advanced Ceramic Materials, Cambridge University Press, Cambridge, 1989.
- G. Huiras, in Ceramic Technology International 1994, ed. I. Birkby, Sterling Publications Limited, Hong Kong, 1993, p. 37.
- J. M. Bind, T. Dupin, J. Schafer and M. Titeux, J. Metals, 1987, **54**, 60.
- D. Caurant, N. Baffier, B. Garcia and J. P. Pereira-Ramos, Solid State Ionics, 1996, 91, 45.
- C. D. Sagel-Ransijn, A. J. A. Winnubst, A. J. Burgraaf and H. Verweij, in Ceramic Transactions, volume 51: Ceramic Processing Science and Technology, ed. H. Hausner, G. L. Messing and S. Hirano, The American Ceramic Society, Westerville, OH, 1995, p. 33.
- 12 D. H. Kerridge, in Chemistry of Non-Aqueous Solvents, ed. J. J. Lagowski, Academic Press, New York, 1978, vol. 5B, p. 269.
- H. Lux, Z. Elektrochem., 1939, 45, 303.
- D. H. Kerridge and J. Cancela Rey, J. Inorg. Nucl. Chem., 1977, **39**, 405.
- H. Al Raihini, B. Durand, F. Chassagneux, D. H. Kerridge and D. Inman, J. Mater. Chem., 1994, 4, 1331.
- Y. Du and D. Inman, J. Mater. Sci., 1996, 31, 5505.
- B. Durand and M. Roubin, Mater. Sci. Forum, 1991, 73-75, 663.
- M. Descemond, C. Brodhag, F. Thevenot, B. Durand, M. Jebrouni and M. Roubin, J. Mater. Sci., 1993, 28, 2283.
- D. Hamon, M. Vrinat, M. Breysse, B. Durand, L. Mosoni, M. Roubin and T. des Couriers, Eur. J. Solid State Inorg. Chem., 1993, 30, 713.
- S. Gopalan, K. Mehta and A. V. Virka, J. Mater. Res., 1996, 11,
- D. H. Everett, Basic Principles of Colloid Science, Royal Society of Chemistry, London, 1988.
- D. L. Segal and J. L. Woodhead, Proc. Br. Ceram. Soc., 1986, 38, 245.
- E. M. Rabinovich, in Sol-Gel Technology for Thin Films, Fibres, Preforms, Electronics and Specialty Shapes, ed. L. C. Klein, Noyes Publications, New Jersey, 1988, p. 260.
- 24 K. Masters, Bull. Am. Ceram. Soc., 1994, 73, 63.
- R. L. Nelson, J. D. F. Ramsay, J. L. Woodhead, J. A. Cairns and J. A. A. Crossley, Thin Solid Films, 1981, 81, 329.
- J. D. Birchall, in Concise Encyclopaedia of Advanced Ceramic Materials, ed. R. J. Brook, Pergamon Press, Oxford, 1991, p. 236.
- H. G. Sowman, Bull. Am. Ceram. Soc., 1988, 67, 1911.
- R. D. Shoup and W. J. Wein, US Pat., 4059658, 1977.
- R. D. Shoup, in Ultrastructure Processing of Advanced Materials, ed. D. R. Uhlmann and D. R. Ulrich, John Wiley and Sons, New York, 1992, p. 291.
- J. Laurie, C. M. Bagnall, B. Harris, R. W. Jones, R. G. Cooke, R. S. Russell-Floyd, T. H. Wang and F. W. Hammett, J. Non-Cryst. Solids, 1992, 147-148, 320.
- L. Bergstrom, in Ceramic Transactions, volume 51: Ceramic Processing Science and Technology, ed. H. Hausner, G. L. Messing and S. Hirano, The American Ceramic Society, Westerville, OH, 1995, p. 341.
- C. F. Baes Jr. and R. E. Mesmer, The Hydrolysis of Cations, John Wiley and Sons, New York, 1976.
- J. Livage, M. Henry and C. Sanchez, Prog. Solid State Chem., 1988, **18**, 259.
- J. Livage, M. Henry and J. P. Jolivet, in Chemical Processing of Advanced Materials, ed. L. L. Hench and J. K. West, John Wiley and Sons, New York, 1992, p. 223.
- C. J. Brinker and G. W. Scherer, Sol-Gel Science. The Physics and Chemistry of Sol-Gel Processing, Academic Press, New York, 1990.
- D. C. Bradley, R. C. Mehrotra and P. D. Gaur, Metal Alkoxides, Academic Press, London, 1978.
- T. J. Leedham, Mater. Res. Soc. Symp. Proc., 1996, 415, 79.
- S. Taketomi, K. Kawasaki, Y. Ozaki, S. Yuasa, Y. Otani and H. Miyajima, J. Am. Ceram. Soc., 1994, 77, 1787.
- J. Livage, F. Babonneau, M. Chatry and L. Coury, Ceram. Int., 1997, **23**, 13.

- W. Stöber, A. Fink and E. Bohn, J. Colloid Interface Sci., 1968, 26, 62.
- 41 H. Giesche, J. Eur. Ceram. Soc., 1994, 14, 205.
- 42 J. L. Look, G. H. Bogush and C. F. Zukoski, *Faraday Discuss.*, 1990, 90, 345.
- 43 M. Ocana, R. R. Clemente and C. J. Serna, Adv. Mater., 1995, 7, 212.
- 44 E. Matijevic, Chem. Mater., 1993, 5, 412.
- 45 A. Patel, D. A. Tossell, N. M. Shorrocks, R. W. Whatmore and R. Watton, *Br. Ceram. Proc.*, 1994, **52**, 77.
- 46 B. A. Tuttle and R. W. Schwartz, MRS Bull., 1996, 21, 49.
- 47 L. C. Klein and N. Giszpenc, Bull. Am. Ceram. Soc., 1990, 69, 1821.
- 48 M. A. Anderson and Q. Xu, US Pat., 5169576, 1992.
- 49 L. Cot, Ch. Guizard and A. Larbot, Ind. Ceram., 1988, 8, 143.
- 50 L. L. Hench and J. K. West, Chem. Rev., 1990, 90, 33.
- 51 J. Fricke and A. Emmerling, J. Am. Ceram. Soc., 1992, 75, 2027.
- 52 D. M. Smith, R. Deshpande and C. J. Brinker, in Ceramic Transactions, volume 31: Porous Materials, ed. K. Ishizaki, L. Sheppard, S. Okada, T. Hamasaki and B. Huybrechts, The American Ceramic Society, Westerville, OH, 1993, p. 71.
- 53 A. B. Brennan, D. E. Rodrigues, B. Wang and G. L. Wilkes, in Chemical Processing of Advanced Materials, ed. L. L. Hench and J. K. West, John Wiley and Sons, New York, 1992, p. 807.
- 54 S. J. Kramer and J. D. Mackenzie, *Mater. Res. Soc. Symp. Proc.*, 1994, **346**, 709.
- 55 H. K. Schmidt, Mater. Res. Soc. Symp. Proc., 1990, 180, 961.
- Materials Research Society Symposium Proceedings: Better Ceramics Through Chemistry VII, Organic/Inorganic Hybrid Materials, volume 434, ed. B. K. Coltrain, C. Sanchez, D. W. Schafer and G. L. Wilkes, Materials Research Society, Pittsburgh, PA, 1996.
- 57 Mater. Sci. Forum: Soft Chemistry Routes to New Materials, volume 152–153, ed. J. Rouxel, M. Tournoux and R. Brec, Trans Tech Publications, Basle, 1994.
- 58 D. Barb, L. Diamandescu, A. Rusi, D. Tarabasani-Mihaila, M. Morariu and V. Teodorescu, J. Mater. Sci., 1986, 21, 1118.
- 59 A. Ataie, I. R. Harris and C. B. Ponton, Br. Ceram. Proc., 1994, 52, 273.
- 60 R. P. Denkewicz Jr., K. S. TenHuisen and J. H. Adair, *J. Mater. Res.*, 1990, 5, 2698.
- 61 R. Basca, P. Ravindranathan and J. P. Dougherty, *J. Mater. Res.*, 1992, 7, 423.
- 62 J. O. Eckart Jr., C. C. Hung-Houston, B. L. Gersten, M. M. Lencka and R. E. Riman, J. Am. Ceram. Soc., 1996, 79, 2929.
- 63 S. Yajima, M. Omori, J. Hayashi, K. Okamuya, T. Matsuzawa and C. Liaw, Chem. Lett., 1976, p. 551.
- 64 S. Yajima, J. Hayashi and M. Omori and K. Okamura, *Nature* (*London*), 1976, **261**, 683.
- 65 D. Seyferth and H. Lang, in *Ultrastructure Processing of Advanced Materials*, ed. D. R. Uhlmann and D. R. Ulrich, John Wiley and Sons, New York, 1992, p. 667.
- 66 R. C. West, L. D. David, P. I. Djurovich, H. Yu and R. Sinclair, Bull. Am. Ceram. Soc., 1983, 62, 899.
- 67 P. Greil, T. Emy and D. Suttor, in *Ceramic Transactions, volume* 51: Ceramic Processing Science and Technology, ed. H. Hausner,

- G. L. Messing and S. Hirano, The American Ceramic Society, Westerville, OH, 1995, p. 171.
- 68 R. Riedel and W. Dressler, Ceram. Int., 1996, 22, 233.
- 69 O. Funayama, T. Aoki, T. Kato, M. Okoda and T. Isoda, *J. Mater. Sci.*, 1996, 31, 6369.
- 70 D. Seyferth and W. S. Rees Jr., Chem. Mater., 1991, 3, 1106.
- 71 M. Seibold and C. Russel, *Mater. Res. Soc. Symp. Proc.*, 1988, 121, 477.
- 72 S. C. Danforth, Nanostruct. Mater., 1992, 1, 197.
- 73 T. Iwai, T. Kawahito and T. Yamada, US Pat., 4196178, 1980.
- 74 C. E. Johnson, D. K. Hickey and D. C. Harris, *Mater. Res. Soc. Symp. Proc.*, 1986, 73, 785.
- 75 A. B. Seddon, S. N. B. Hodgson and M. G. Scott, *J. Mater. Sci.*, 1991, **26**, 2599.
- 76 R. J. P. Corriu, D. Leclercq, P. Lefevre, P. Hubert-Mutin and A. Vioux, J. Mater. Chem., 1992, 2, 673.
- 77 P. Arnal, R. J. P. Corriu, D. Leclercq, P. Hubert-Mutin and A. Vioux, Mater. Res. Soc. Symp. Proc., 1994, 346, 339.
- T. D. Xiao, K. E. Gonsalves, P. R. Strutt and P. G. Klemens, J. Mater. Sci., 1993, 28, 1334.
- 79 G. L. Messing, S. C. Zhang and G. V. Jayanthi, J. Am. Ceram. Soc., 1993, 76, 2707.
- 80 D. L. Segal and A. Atkinson, Br. Ceram. Trans., 1996, 95, 103.
- 81 Y. Senzaki, J. Caruso, M. J. Hampden-Smith, T. T. Kodas and L-M. Wang, J. Am. Ceram. Soc., 1995, 78, 2973.
- 82 E. B. Slamovich and F. F. Lange, Mater. Res. Soc. Symp. Proc., 1988, 121, 257.
- 83 M. J. Ruthner, Mater. Sci. Monogr., 1983, 16, 515.
- 84 G. W. Kriechbaum and P. Kleinschmit, Adv. Mater., 1989, 2, 330.
- 85 W. R. Cannon, S. C. Danforth, J. H. Flint, J. S. Haggerty and R. A. Marra, J. Am. Ceram. Soc., 1982, 65, 324.
- 86 Y. Li, Y. Liang, F. Zheng and Z. Hu, Mater. Sci. Eng. A, 1994, 174, L23.
- 87 S. R. Blackburn, T. A. Egerton and A. G. Jones, *Br. Ceram. Soc.*, 1991, 47, 87.
- 38 M. P. Pechini, US Pat., 3 330 697, 1967.
- 89 N. G. Eror and H. U. Anderson, Mater. Res. Soc. Symp. Proc., 1986, 73, 571.
- C. Marcilly, P. Courty and B. Delmon, J. Am. Ceram. Soc., 1970, 53, 56.
- 91 Y. G. Metlin and Y. D. Tretyakov, J. Mater. Chem., 1994, 4, 1659.
- D. H. A. Blank, H. Kruidhof and J. Flokstra, *J. Phys. D: Appl. Phys.*, 1988, 226.
- 93 Y. S. Lin and Y. Zeng, J. Catal., 1996, 164, 220.
- 94 M. Arima, M. Kakihana, Y. Nakamura, M. Yashima and M. Yoshimura, J. Am. Ceram. Soc., 1996, 79, 2847.
- L. Liz, M. A. Lopez Quintela, J. Mira and J. Rivas, J. Mater. Sci., 1994, 29, 3797.
- 96 P. D. Moran, J. R. Bartlett, J. L. Woolfrey, G. A. Bowmaker and R. P. Cooney, in *Ceramic Transactions, volume 51: Ceramic Processing Science and Technology*, ed. H. Hausner, G. L. Messing and S. Hirano, The American Ceramic Society, Westerville, OH, 1995, p. 27.

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